

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
8 March 2001 (08.03.2001)

PCT

(10) International Publication Number
WO 01/16642 A2

(51) International Patent Classification ⁷ :	G02F	US	09/614,195 (CIP)
		Filed on	12 July 2000 (12.07.2000)
(21) International Application Number:	PCT/US00/22831	US	09/614,375 (CIP)
		Filed on	12 July 2000 (12.07.2000)
(22) International Filing Date:	18 August 2000 (18.08.2000)	US	09/614,865 (CIP)
		Filed on	12 July 2000 (12.07.2000)
(25) Filing Language:	English	US	09/614,224 (CIP)
		Filed on	12 July 2000 (12.07.2000)
(26) Publication Language:	English	(71) Applicant (<i>for all designated States except US</i>): AGILITY COMMUNICATIONS, INC. [US/US]; 5385 Hollister Avenue, Suite 309, Santa Barbara, CA 93111 (US).	
(30) Priority Data:		(72) Inventor; and	
60/152,072	2 September 1999 (02.09.1999)	US	(75) Inventor/Applicant (<i>for US only</i>): COLDREN, Larry, A. [US/US]; 4665 Via Vistosa, Santa Barbara, CA 93110 (US).
60/152,049	2 September 1999 (02.09.1999)	US	
60/152,038	2 September 1999 (02.09.1999)	US	
09/614,377	12 July 2000 (12.07.2000)	US	(74) Agent: DAVIS, Paul; Wilson Sonsini Goodrich & Rosati, 650 Page Mill Road, Palo Alto, CA 94304-1050 (US).
09/614,895	12 July 2000 (12.07.2000)	US	
09/614,674	12 July 2000 (12.07.2000)	US	
09/614,378	12 July 2000 (12.07.2000)	US	(81) Designated States (<i>national</i>): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BR, BY, BZ, CA, CH, CN, CR, CU, CZ, DE, DK, DM, DZ, EE, ES, FI, GB, GD, GE, GH, GM, HR, HU, ID, IL, IN, IS, JP, KE, KG, KP, KR, KZ, LC, LK, LR, LS, LT, LU, LV, MA, MD, MG, MK, MN, MW, MX, MZ, NO, NZ, PL, PT, RO, RU, SD, SE, SG, SI, SK, SL, TJ, TM, TR, TT, TZ, UA, UG, US, UZ, VN, YU, ZA, ZW.
09/614,376	12 July 2000 (12.07.2000)	US	
09/614,195	12 July 2000 (12.07.2000)	US	
09/614,375	12 July 2000 (12.07.2000)	US	
09/614,865	12 July 2000 (12.07.2000)	US	
09/614,224	12 July 2000 (12.07.2000)	US	
(63) Related by continuation (CON) or continuation-in-part (CIP) to earlier applications:		(84) Designated States (<i>regional</i>): ARIPO patent (GH, GM, KE, LS, MW, MZ, SD, SL, SZ, TZ, UG, ZW), Eurasian patent (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, GW, ML, MR, NE, SN, TD, TG).	
US	60/152,072 (CIP)		
Filed on	2 September 1999 (02.09.1999)		
US	60/152,049 (CIP)		
Filed on	2 September 1999 (02.09.1999)		
US	60/152,038 (CIP)		
Filed on	2 September 1999 (02.09.1999)		
US	09/614,377 (CIP)		
Filed on	12 July 2000 (12.07.2000)		
US	09/614,895 (CIP)		
Filed on	12 July 2000 (12.07.2000)		
US	09/614,674 (CIP)		
Filed on	12 July 2000 (12.07.2000)		
US	09/614,378 (CIP)		
Filed on	12 July 2000 (12.07.2000)		
US	09/614,376 (CIP)		
Filed on	12 July 2000 (12.07.2000)		

Published:

— *Without international search report and to be republished upon receipt of that report.*

For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

WO 01/16642 A2

(54) Title: INTEGRATED OPTO-ELECTRONIC WAVELENGTH CONVERTER ASSEMBLY

(57) Abstract: A wavelength converter assembly includes a substrate. An epitaxial structure is formed on the substrate with areas of different optical properties. A laser and a photodetector are formed in the epitaxial structure. The photodetector generates a first electrical signal in response to an optical signal. A conditioning circuit is coupled to the laser and the photodetector. The conditioning circuit receives the first electrical signal and provides a second electrical signal to the laser to modulate its optical output.

INTEGRATED OPTO-ELECTRONIC WAVELENGTH CONVERTER ASSEMBLY

BACKGROUND OF THE INVENTION

5 Field of the Invention

This invention relates to wavelength converters of the type desirable in certain wavelength division multiplexed optical communication networks, as well as other applications where it is desirable to change the wavelength of the optical carrier of a modulated lightwave, and more particularly to optoelectronic 10 wavelength converters in which an incoming lightwave having a first wavelength is detected by a photodetector that produces an electrical signal that in turn modulates a source of an outgoing lightwave having a desired second wavelength.

15 Description of the Related Art

Optoelectronic wavelength conversion processes have used as separate photodetectors, receiver and regeneration circuits, transmitter and driver circuits, and directly or externally modulated lasers. S.J.B. Yoo, "Wavelength conversion technologies for WDM network applications," *J. Lightwave Techn.* 20 14 (6) (June, 1996). These discrete-component wavelength converters have tended to be relatively bulky and expensive to manufacture. Also, the lasers generally have a fixed wavelength or a very limited tuning range.

There is a need for a monolithic wavelength converter assembly that provides for the process of detection and regeneration at some other 25 wavelength. There is a need for a monolithic wavelength converter assembly fabricated on one semiconductor substrate using compatible photonic integrated circuit technology for all components. There is a further need for a wavelength converter assembly where signal amplification is obtained without the use of electronic transistors. There is yet a further need for a wavelength converter 30 assembly where conditioning of the signal is done in combination with the detection or modulation process in the optical or electrical domain. There is still a further need for a wavelength converter assembly that has a wide tuning

range and all of the components are fabricated on one semiconductor substrate using compatible photonic integrated circuit technology.

BRIEF DESCRIPTION OF THE FIGURES

5 Figure 1 is a block diagram of one embodiment of a wavelength converter assembly of the present invention.

Figure 2(a) is a top down schematic view of a waveguide photodetector that can be part of the Figure 1 wavelength converter assembly.

10 Figure 2(b) is a top down schematic view of a waveguide photodetector that can be part of the Figure 1 wavelength converter assembly.

Figure 2(c) is a top down schematic view of waveguide photodetector integrated with a semiconductor-optical amplifier (“SOA”) preamplifier that can be part of the Figure 1 wavelength converter assembly.

15 Figure 2(d) is a top down schematic view of a waveguide photodetector integrated with a SOA preamplifier and a tunable resonant-cavity filter that can be part of the Figure 1 wavelength converter assembly.

Figure 3(a) is a cross sectional view of the semiconductor layer structure of the Figure 2(d) assembly in which passive sections are created by removal of the active regions prior to regrowth.

20 Figure 3(b) is a cross sectional view of the semiconductor layer structure of the Figure 2(d) assembly in which passive sections are created by variable thickness and composition quantum-wells via intermixing after uniform growth or selective area growth.

25 Figure 4(a) is a schematic top down view of a sampled-grating distributed-Bragg-reflector (“SGDBR”) tunable laser having a series-connected, axially segmented multiple-active region that can be part of the Figure 1 wavelength converter assembly.

Figure 4(b) is a schematic of a SGDBR tunable laser that has a series-connected, vertically stacked multiple-active region that can be part of the Figure 1 wavelength converter assembly.

30 Figure 4(c) is a schematic top down view of a SGDBR tunable laser with an integrated external SOA that can be part of the Figure 1 wavelength converter assembly.

Figure 4(d) is a schematic top down view of a SGDBR tunable laser with an integrated external electro-absorption modulator (EAM) and two SOAs that can be part of the Figure 1 wavelength converter assembly..

5 Figure 5(a) is a cross sectional view of the Figure 4(a) structure.

Figure 5(b) is a cross sectional view of the Figure 4(b) structure.

Figure 6 is schematic diagram of an equivalent circuit that can be used with the structures of Figures 2(a), 2(b), 4(a) and 4(b) as well as an integrable current conditioning circuit.

10 Figure 7 is a plot of the desired impedance of the Figure 1 nonlinear current conditioning circuit.

Figures 8(a) and (b) illustrate an embodiment of a monolithic wavelength converter assembly of the present invention where the photodetector is integrated directly on top of the laser.

15 SUMMARY OF THE INVENTION

Accordingly, an object of the present invention is to provide an improved wavelength converter assembly.

Another object of the present invention is to provide monolithic wavelength converter assembly that provides for the process of detection and 20 regeneration at some other wavelength.

A further object of the present invention is to provide a monolithic wavelength converter assembly fabricated on one semiconductor substrate using compatible photonic integrated circuit technology for all components.

Yet another object of the present invention is to provide a wavelength 25 converter assembly where signal amplification is obtained without the use of electronic transistors.

Another object of the present invention is to provide a wavelength converter assembly where conditioning of the signal is done in combination with the detection or modulation process in the optical or electrical domain.

30 A further object of the present invention is to provide a wavelength converter assembly that has a wide tuning range and all of the components are fabricated on one semiconductor substrate using compatible photonic integrated circuit technology.

Yet a further object of the present invention is to provide a monolithic wavelength converter assembly that provides high data bandwidths.

Another object of the present invention is to provide a monolithic wavelength converter assembly that provides a large output optical signal
5 amplitude without the need for integrated transistors for electronic amplification.

Still a further object of the present invention is to provide a monolithic wavelength converter assembly that provides conditioned output data waveforms with lower noise and distortion than at an input.

10 Another object of the present invention is to provide a monolithic wavelength converter assembly that can be extended to large arrays of wavelength converters integrated on one substrate with photonic integrated circuit technology.

These and other objects of the present invention are achieved in a
15 wavelength converter assembly that includes a substrate. An epitaxial structure is formed on the substrate with areas of different optical properties. A laser and a photodetector are formed in the epitaxial structure. The photodetector generates a first electrical signal in response to an optical signal. A conditioning circuit is coupled to the laser and the photodetector. The
20 conditioning circuit receives the first electrical signal and provides a second electrical signal to the laser to modulate its optical output.

In another embodiment of the present invention, a wavelength converter assembly includes first and second semiconductor layers formed in an epitaxial structure. The first and second semiconductor layers having different dopings.
25 A first waveguide layer is formed between the first and second semiconductor layers. The first waveguide layer includes first and second reflectors that define a resonant cavity. An optically active gain medium is disposed between the first and second reflectors. A photodetector is formed on the first semiconductor layer and includes an optically active absorber region. The photodetector generates a first electrical signal in response to an optical input.
30

DETAILED DESCRIPTION

Referring now to Figure 1, a wavelength converter assembly 10 of the present invention provides for the process of detection and regeneration at some other wavelength to be carried out with a monolithic apparatus. Wavelength converter assembly 10 is fabricated on one semiconductor substrate using compatible photonic integrated circuit (IC) technology for all components. An advantage of wavelength converter assembly 10 over other devices is that signal amplification is obtained without the use of electronic transistors, which would involve incompatible fabrication technology. Moreover, the conditioning of the signal may be done in combination with the detection or modulation process in the optical or electrical domain. Laser output from wavelength converter assembly 10 can have a wide tuning range so that a large number of output wavelengths are possible.

In one embodiment, the elements of wavelength converter assembly 10 are fabricated on a single wafer. The various elements are derived from a common epitaxial layer structure, and are fabricated by common process steps.

Monolithic integration of optically dissimilar elements is accomplished by a method of fabrication that tailors optical properties of selected regions to a desired electro-optic function. Tailored optical properties, including the band gap, result in optically active and passive regions on the same wafer beginning from a common epitaxial layer structure. Further, the common fabrication process steps required for forming the apparatus elements are compatible with photonic device fabrication processes presently used in the lightwave industry. Thus, wavelength converter assembly 10 is readily manufacturable.

In a particular embodiment, the fabrication methods to selectively tailor the band gaps of regions of the wafer of wavelength converter assembly 10 include the steps of, implantation of impurities by low energy ions (less than about 200 eV) in a portion of a selected wafer region near the wafer surface; and annealing the wafer. This allows the impurities and vacancies implanted near the wafer surface to diffuse throughout the selected region and tailor the region's band gap to a desired electro-optic function.

For example, in the passive waveguide regions of the phase shift and mirror sections of a tunable laser element 12, the effective bandgap should be somewhat larger (e.g., > 0.1 eV) than the operating lightwave energy, which is only slightly larger (typically ~ 0.01- 0.05 eV) than the effective bandgap of the active layers in the gain section. Integrated external modulator elements may have sections with the same larger bandgap as the other passive regions, or a bandgap intermediate between that of the active and passive sections for some desired functionality such as chirp reduction or improved -linearity. Integrated external amplifier elements (M. J. O'Mahony, "Semiconductor laser Optical Amplifiers for Use in Future Fiber Systems," *J. Lightwave Techn.* 6 (4) (April, 1988.); A. E. Kelly, I. F. Lealman, L. J. Rivers, S. D. Perrin, and M. Silver, "Low noise figure (7.2 dB) and high gain (29dB) semiconductor optical amplifier with a single layer AR coating," *Electron. Lett.*, 33 pp 536-8 (1997.)) may have the same bandgap as the active gain section or a slightly modified bandgap for some functionality, such as increased saturation power or improved chirp of modulator/amplifier combinations. Robert G. Walker, "High-Speed III-V Semiconductor Intensity Modulators," *IEEE J. Quant. Electron.*, 27, (3), 654-667, (March 1991); F. Koyama and K. Iga, "Frequency Chirping in External Modulators," *J. Lightwave Tech.*, 6 (1), 87-93, (January 1988).

In various embodiments of the present invention, the passive regions are created by selective removal of the lowest bandgap layers responsible for gain in the active regions within the same sequence as some other processing steps, such as grating formation in the mirror regions, are being carried out. B. Mason, G.A. Fish, S.P. DenBaars, and L.A. Coldren, "Widely Tunable Sampled Grating DBR Laser with Integrated Electroabsorption Modulator," *Photon. Tech. Letts.*, 11, (6), 638-640, (June 1999). In such cases the ion-implantation process is not necessary, but it may be utilized to better tailor other regions such as in integrated modulators and/or amplifier elements. This sequence is followed by a regrowth of the upper cladding layers required for the top portion of the optical waveguide.

According to aspects of the present invention, the data signal is available in electrical form for monitoring, tapping, and modification. In particular, a packet address or header information can be read and used to determine the

routing of the information either by selection of the output wavelength or by setting the state of some switch that might follow the wavelength converter assembly. These and other desirable features are all incorporated within novel, monolithically-integrated optoelectronic wavelength converter assembly
5 structures that make use of a manufacturable, integrated photonic IC technology. G.A. Fish, B. Mason, L.A. Coldren, and S.P. DenBaars, "Compact 1.55 μ m Spot-Size Converters for Photonic Integrated Circuits," *Integrated Photonics Research '99*, Santa Barbara, CA, paper no. RWD4, 375-377, (July 19-21, 1999).

10 Further features of wavelength converter assembly 10 include but are not limited to,: 1.) providing higher data bandwidths than currently available from currently available devices (T. Ido, S. Tanaka, M. Suzuki, M. Koizumi, H. Sano, and H. Inoue, "Ultra-High-Speed Multiple-Quantum-Well Electro-Absorption Optical Modulators with Integrated Waveguides," *J. Lightwave Techn.*, 14, (9), 2026-2034, (September 1996)), 2) providing a wider range of
15 possible output wavelengths than currently available devices (V. Jayaraman, A. Mathur, L.A. Coldren and P.D. Dapkus, "Theory, Design, and Performance of Extended Tuning Range in Sampled Grating DBR Lasers," *IEEE J. Quantum Elec.*, 29, (6), 1824-1834, (June 1993)), 3.) providing equal or larger output
20 optical signal amplitude than current devices without the need for integrated transistors for electronic amplification (J.K. Kim, E. Hall, O. Sjölund, and L.A. Coldren, "Epitaxially-Stacked Multiple-Active-Region 1.55 μ m Lasers for Increased Differential Efficiency," *Appl. Phys. Letts.*, 74, (22) 3251-3253, (May 31, 1999); J.T. Getty, O. Buchinsky, R.A. Slavatore, B. Mason, P.G. Piva, S.
25 Charbonneau, K.S. Grabowski, and L.A. Coldren, "Monolithic Series-Connected 1.55 μ m Segmented-Ridge Lasers," *Electronics Letters*, 35, (15), 1257-1258, (July 22, 1999)), 4.) providing conditioned output data waveforms having lower noise and distortion than at the input and 5.) providing capabilities
for extensions to large arrays of such wavelength converters, the arrays
30 integrated on one substrate with existing photonic IC technology. Coldren, L., "Diode Lasers and Photonic Integrated Circuits," Wiley, (1995).

Figure 1 illustrates certain generic elements, in block diagram form, of wavelength converter assembly 10. Illustrated are a multisection tunable laser

element 12 (hereafter referred to as "laser 12"), a photodetector element 14 (hereafter referred to as "photodetector 14" and a current conditioning circuit element 16. The insets in the blocks are suggestive of the possible contents of elements 12, 14 and 16. Current from photodetector 14 modulates the laser 12 after being conditioned by the conditioning circuit. The net functionality provides wavelength conversion of an optical carrier modulated with some data such that: i) an arbitrary output wavelength within a band can be emitted; ii) the amplitude of the output can be adjusted within a useful range; and, iii) the noise and distortion on the data can be reduced. An important aspect of the invention is integration with a common photonic IC technology that has been described in F. Koyama and K. Iga, "Frequency Chirping in External Modulators," *J. Lightwave Tech.*, 6 (1), 87-93, (January 1988); B. Mason, G.A. Fish, S.P. DenBaars, and L.A. Coldren, "Widely Tunable Sampled Grating DBR Laser with Integrated Electroabsorption Modulator," *Photon. Tech. Letts.*, 11, (6), 638-640, (June 1999). Moreover, integration of elements 12, 14 and 16 provides an advantageous functionality that is not possible by interconnecting discrete elements using conventional printed circuit board or multi-chip module technology. Additionally, integration of elements 12, 14 and 16 enables low-cost, high-yield manufacturing processes to be used.

As illustrated in Figure 1, laser 12 can include first and second SGDBR's 18 and 20, a first and second SOA's 22 and 24 and EAM 26 and a multiple active region, MAR 28. Photodetector element 16 can include an SOA 30, first and second filters 32 and 34 and an absorber 36.

Wavelength converter 10 offers a number of advantages. In the embodiment illustrated in Figure 2(a), the surface-illuminated geometry photodetector 14 enables efficient and polarization independent coupling of light from optical fibers to absorber 36 of photodiode 12. Moreover, it does not require a large footprint on the substrate, and its modest dimensions, in one embodiment approximately 10- 30 μm in diameter, provide for high bandwidth, sensitive operation. In various embodiments, the sensitivity of wavelength converter assembly 10 can be enhanced by incorporation of a multi-layer reflective stack beneath the wavelength converter assembly 10 to create a resonant-cavity photodiode 14. This stack forms the lower cladding region of

laser 12 without any complication. As in other embodiments, surface-illuminated photodiode 14 is isolated by a proton and/or He⁺ ion implantation or other means well known to those skilled in the art, rendering the surrounding areas semi-insulating. In particular embodiments, the bottom contact of wavelength converter assembly 10 is brought out to the side for biasing and the top contact is directly interconnected to laser 12 with a shunt branch to conditioning circuit 16.

A waveguide layer structure of photodetector 14 illustrated is Figure 2(b) is identical to the gain section of laser 12. In this embodiment, the waveguide layer structure of photodetector 14 provides for higher saturation power than typical surface-illuminated designs. Optical coupling to the waveguide can be enhanced by the integration of compatible mode transformers using techniques such as those described in G.A. Fish, B. Mason, L.A. Coldren, and S.P. DenBaars, "Compact 1.55μm Spot-Size Converters for Photonic Integrated Circuits," *Integrated Photonics Research '99*, Santa Barbara, CA, paper no. RWD4, 375-377, (July 19-21, 1999). For ultra high bandwidth embodiments, such as for example greater than 50 GHz, a terminated traveling wave electrode structure may be incorporated. A suitable traveling wave electrode structure is described in 8. T. Ido, S. Tanaka, M. Suzuki, M. Koizumi, H. Sano, and H. Inoue, "Ultra-High-Speed Multiple-Quantum-Well Electro-Absorption Optical Modulators with Integrated Waveguides," *J. Lightwave Techn.*, 14, (9), 2026-2034, (September 1996).

Referring now to Figure 2(c), the addition of an optical preamplifier, SOA 30, increases the optical signal incident on absorber section 36 and provides higher output photocurrent. This is advantageous by allowing the use of low-level data while still obtaining sufficient current to properly modulate laser 12 and also allows for data regeneration by a shunt conditioning circuit. SOA 30 can also provide for signal level adjustment in conjunction with an external control circuit. Noise added by SOA 30 may be removed by current conditioning circuit 18, resulting in a noise figure that does not degrade the data. The layer structure of SOA 30 can be identical to the gain section of laser 12.

If the signal to noise level is low, or if unwanted data at another wavelength is present in the input lightwave, or if a shorter absorber section is desired, it may be advantageous to place absorber 36 within a resonant cavity to filter out unwanted signals out-of-band. As illustrated in Figure 2(d),

5 photodetector 14 is integrated with SOA 30 and a tunable resonant-cavity filter. This waveguide geometry reflects light signals that are not within the resonant bandwidth of the resonant cavity formed by two DBR's 38 and 40 and enhances the signal. A shorter absorber length may be used for total absorption and high quantum efficiency. This shortened length, in turn, reduces photodetector's 14

10 capacitance, enabling very high bandwidth operation.

Figures 3(a) and 3(b) are cross-sectional views of the semiconductor layer waveguide structure of the Figure 2(d) photodetector 14. In Figure 3(a) passive sections are created by removal of the active regions prior to regrowth. In Figure 3(b) passive sections are created by variable thickness and

15 composition quantum-wells via intermixing after uniform growth or selective area growth. Figure 3(a) and 3(b) illustrate that waveguide photodetectors 14 are compatible with the tunable sections of laser 12 that are illustrated in Figure 5. It will be appreciated that various sections shown in Figures 3(a) and 3(b) are omitted in the Figure 2(a), 2(b) and 2(c) embodiments.

20 Figures 4(a) and 5(a) illustrate embodiments of wavelength converter assembly 10 with a series-connected, axially segmented active region that obtains signal gain within a widely tunable SGDBR laser 12 as described in United States Patent 4,896,325. The principle of operation of each SGDBR 18 and 20 is well known to those skilled in the art, as is the concept of using MAR 25 28 within a single optical cavity to obtain a differential efficiency greater than unity.

Figures 4(b) and 5(b) illustrate another embodiment employing the same concepts. In this embodiment, the separate *pin* active regions of the gain section are integrated vertically with the series electrical connections derived from intermediate n^+ - p^+ tunnel diodes. This layer structure is particularly useful in combination with the vertical resonant-cavity photodiode embodiment of Figure 2(a), since more absorption can lead to photodiodes with broader optical bandwidth and better efficiency as well. Absorbers can be placed at

standing wave peaks and the tunnel diodes at standing wave nulls to provide a multiplication in absorbency by nearly 2x the number of active regions.

Figure 4(c) illustrates another embodiment of the invention. In Figure 4(c), the signal gain is enhanced relative to other embodiments by the addition 5 of integrated SOA 22 external to the laser cavity. The data signal current is still applied to the gain section, and the gain section may either be of a conventional single active region, or MAR 28, as in Figure 4(a) or 4(b) embodiments, for more signal gain. External SOA 22 can provide about 20 dB of gain, whereas the multiple active region design provides for roughly unity gain. Normal lasers 10 have differential efficiencies ~ 20 – 30 %; thus the MAR 28 design gives about 3 to 5x enhancement. The MAR 28 design is advantageous because it does not degrade the signal-to-noise ratio, whereas SOA 22 does. However, if the signal level is already high, as it can be with a MAR gain section and/or gain in photodetector 14, the constant noise added by SOA 22 can be negligible. This 15 geometry also allows for the leveling of the output data signal level via an external control circuit.

If the signal bandwidth is very high, such as but not limited to 15GHz or greater, direct modulation of laser 12 may be difficult. Also, if chirping of the wavelength is a problem, direct modulation may not be an optimal solution. 20 Finally, if the output wavelength of laser 12 must be set very accurately, direct modulation may compromise the ability of control circuit 16 to hold the wavelength with sufficient accuracy. For all of these reasons, use of external modulation, such as illustrated in Figure 4(d), may be desired. In this case, the data signal current is applied to the integrated external modulator. An EAM 44 25 is shown, but an interferometric modulator, such as a Mach-Zehender or directional coupler modulator or other equivalent, is also possible by using passive waveguide sections of appropriate design. As indicated, SOA's 22 and 24 may also be advantageously employed to increase the input carrier level and output modulated data. Use of MAR 28 actives may also be advantageous if 30 laser RIN is to be minimized. Since the active region can be biased by a high-impedance source in this case, no low-source-impedance high-frequency signal, the inherent noise on laser 12 output can be reduced to sub-shot noise levels. SOA's 22 and 24 at laser's 12 output can be avoided by accomplishing the

desired signal gain in photodetector 14 where their noise may be removed by the current conditioning circuit. This provides for signal gain, with a maximal signal-to-noise ratio.

In many embodiments, the current conditioning circuit 16 can be easily created in Si-CMOS if external shunting circuits are used. However, for high-speed operation, the packaging may not provide sufficiently low shunt capacitance, so at least some of the functionality may be desirable to have on-chip. The shunt impedance of this circuit is shown in Figure 7. With this circuit shunting the drive current, noise on the baseline (logical '0') and maximum (logical '1') of the data can be removed, provided that the signal level can be adjusted to the appropriate levels by the gain components in photodetector 14.

One embodiment of an integrable conditioning circuit 16 for the laser bias is shown in Figure 6. Diode chains can be used to threshold and limit the level of the modulating data signal. These can be integrated using the same fabrication steps already necessary to create photodetector 14 and tunable elements of laser 12 shown in Figures 2 through 5.

Other conditioning circuits are possible that provide the characteristic of Figure 7 and the desired laser active region (gain) or EAM bias using compatible integrable technology, and these can be obtained by using standard circuit design packages. If the photocurrent is to be applied to the EAM, such as may be desired for high-speed operation, then current conditioning circuit 16 may supply the correct reverse bias voltage to the EAM for some desired operation. Such desired operations include but are not limited to minimizing the chirp or maximizing the linearity for an output wavelength from laser 12.

Wavelength converter assembly 10 is a monolithically integrated opto-electronic wavelength converter assembly. Particular embodiments comprise: photodetector 14 electrically coupled to a multi-section, laser 12 having a differential efficiency greater than unity, where the photocurrent can be conditioned by a circuit element to provide tapping, thresholding, and limiting of the detected data. Key elements of circuit conditioning circuit 16 can be integrable with the same fabrication steps required for photodetector 14 and laser 12.

In certain embodiments, photodetector 14 is an edge-illuminated waveguide photodetector. In other embodiments, photodetector 14 is a surface-illuminated element. In the waveguide embodiments, SOA 30 may be integrated with photodetector 14 using the same fabrication sequence for 5 additional gain or level control. In these embodiments, tunable waveguide filter 42 may also be incorporated with the same fabrication sequence to filter out unwanted signals or noise from SOA 30.

Laser 12 can use SGDBR's 18 and 20 and gain and phase-shift sections to provide for output wavelength tunability over a range of several tens of 10 nanometers. To accomplish net signal gain, the gain section of laser 12 may contain several active regions that are driven electrically in series, and/or laser 12 may incorporate an integrated external SOA at its output port.

In a particular embodiment, the conditioned photocurrent is connected to 15 an integrated external modulator to provide reduced wavelength chirping and generally enable higher data rate operation than feasible with direct modulation of the gain section of laser 12. Electro-absorption modulators (EAMs) (Robert G. Walker, "High-Speed III-V Semiconductor Intensity Modulators," *IEEE J. Quant. Electron.*, 27, (3), 654-667, (March 1991); F. Koyama and K. Iga, "Frequency Chirping in External Modulators," *J. Lightwave Tech.*, 6 (1), 87-93, 20 (January 1988); B. Mason, G.A. Fish, S.P. DenBaars, and L.A. Coldren, "Widely Tunable Sampled Grating DBR Laser with Integrated Electroabsorption Modulator," *Photon. Tech. Letts.*, 11, (6), 638-640, (June 1999)) or interferometric modulators can be integrated within the same 25 fabrication sequence as the other elements. In this particular embodiment, SOA sections precede and/or follow the modulator section to accomplish net signal gain and/or data level adjustment. In addition, the combined dispersion characteristics of the SOAs and EAM can be used to provide a desired net chirp characteristic.

In other embodiments, current conditioning circuit element 16 is non-linear and consists of a connection to an external source to supply laser 12 with 30 a necessary threshold current. In another embodiment, current conditioning circuit 16 includes a microwave filter to remove subcarrier header information. In still another embodiment, current conditioning circuit 16 can comprise a

limiting circuit to shunt off any currents above a given level. Current conditioning circuit element 16 can also comprise a thresholding circuit to shunt away photocurrent below a given level. These latter circuits may be partially external to the monolithic photonic IC, or they may comprise appropriate series diode chains that can be compatibly integrated.

All or some of the elements of wavelength converter assembly 10 can be created with a standardized photonic IC fabrication processes. Thus, various options can be added dependant only upon the desired specifications and without the need to develop a new or incompatible materials growth and device fabrication sequence. In one specific embodiment, wavelength converter assembly 10 includes elements that are based on InP substrates, which can provide wavelength conversion and other functionality near the 1.55 μm wavelength band. It will be appreciated that wavelength converter assembly 10 can use other material platforms.

Another embodiment of wavelength converter assembly 10 is illustrated in Figures 8(a) and (b). In this embodiment, metal interconnects between photodetector 14 and laser 12 are avoided by integrating photodetector 14 directly on top of laser 12. This eliminates any excess series resistance or inductance or shunt capacitance between the input and output stages and optimizes the configuration for high-data rate operation. Semi-insulating regrowth of a buried-heterostructure waveguide is also illustrated for high-speed operation. Current conditioning circuit 16 can also be connected by contacting to the intermediate p-InGaAsP layer between vertically stacked photodetector 14 and laser 12. As illustrated, the connection is directly to the integrated modulator, which can be the preferred connection for high-speed low-chirp operation. Vertical illumination is also illustrated, but a horizontal waveguide detector configuration is also possible. The vertical configuration may be preferred since there is less crosstalk between input and output lightwave signals. Such vertical integration is obtained by performing several regrowth steps as is common in such photonic integrated circuits using techniques well known to those skilled in the art.

In one mode of operation of the Figures 8(a) and (b) embodiment, a reverse bias voltage is applied between bias-1 and bias-2 electrodes to deplete

the InGaAs absorber region and provide minimal sweep out times for photocarriers. Bias-2 would be set to the voltage appropriate for optimal operation of the modulator. Example dc potentials include but are not limited to, - 2 V on bias-2 electrode and - 6 V on bias-1 electrode. The thickness of the
5 InGaAs absorber is adjusted to be sufficient to absorb most of the incoming light but not so thick as to slow the transit of carriers to the contact layers. It will be appreciated that an avalanche photodetector (APD) may also be used in place of the simple pin detector indicated in Figures 8(a) and (b). In this case additional layers are desired to optimize the gain-bandwidth product of the
10 APD.

The foregoing description of a preferred embodiment of the invention has been presented for purposes of illustration and description. It is not intended to be exhaustive or to limit the invention to the precise forms disclosed. Obviously, many modifications and variations will be apparent to
15 practitioners skilled in this art. It is intended that the scope of the invention be defined by the following claims and their equivalents.

20

25

30

What is claimed is:

CLAIMS

1. A wavelength converter assembly, comprising:
 - 5 a substrate;
 - an epitaxial structure formed on the substrate with areas of different optical properties;
 - a laser formed in the epitaxial structure;
 - 10 a photodetector formed in the epitaxial structure and coupled to the laser, the photodetector generating a first electrical signal in response to an optical signal;
 - a conditioning circuit coupled to the laser and the photodetector, the conditioning circuit receiving the first electrical signal and providing a second electrical signal to the laser to modulate its optical output.
- 15 2. The assembly of claim 1, wherein the laser is a semiconductor laser.
3. The assembly of claim 1, wherein the conditioning circuit is formed on the substrate.
4. The assembly of claim 3, wherein the conditioning circuit provides necessary bias voltages to the photodetector and laser.
- 20 5. The assembly of claim 3, wherein the conditioning circuit contains nonlinear circuit elements to limit a magnitude of the second electrical signal wherein a maxima of signal pulses are reshaped.
6. The assembly of claim 3, wherein the conditioning circuit contains nonlinear circuit elements to supply a minimum level to the second electrical signal wherein a minima of signal pulses are reshaped.
- 25 7. The assembly of claim 6, wherein the substrate is semi-insulating InP.
8. The assembly of claim 1, wherein the photodetector has at least one bandgap that is different from at least one bandgap of the laser.
- 30 9. The assembly of claim 1, wherein the laser includes a mode tuning element.

10. The assembly of claim 9, wherein the mode tuning element is a controllable phase shifting element.
11. The assembly of claim 1, wherein the laser includes a first reflector and a second reflector that define a resonant cavity, wherein at least one of the first and second reflectors is frequency selective and tunable.
5
12. The assembly of claim 11, wherein at least one of the first and second reflectors is a distributed reflector.
13. The assembly of claim 11, wherein both of the first and second reflectors is a distributed reflector.
10
14. The assembly of claim 11, wherein at least one of the first and second reflectors is a sample grating distributed Bragg reflector.
15. The assembly of claim 11, wherein each of the first and second reflectors is a sample grating distributed Bragg reflector.
16. The assembly of claim 11, wherein a maximum reflectivity of at least one of the first and second reflectors is tunable.
15
17. The assembly of claim 11, wherein a maximum reflectivity of each of the first and second reflectors is tunable.
18. The assembly of claim 11, wherein the maximum reflectivities of each of the first and second reflectors are tunable relative to each other.
20
19. The assembly of claim 1, wherein laser has a gain medium that is coupled to the photodetector.
20. The assembly of claim 1, wherein the laser has a multi-active region gain medium.
21. The assembly of claim 11, wherein the laser includes a controllable amplifier positioned outside of the resonant cavity
25
22. The assembly of claim 11, wherein the laser includes a controllable modulator positioned outside of the resonant cavity.
23. The assembly of claim 11, wherein the laser includes a modulator and at least one amplifier positioned outside of the resonant cavity.
24. The assembly of claim 22, wherein the modulator is coupled to the photodetector wherein the second electrical signal modulates the laser's output with the modulator.
30

25. The assembly of claim 23, wherein the modulator is coupled to the photodetector wherein the second electrical signal modulates the laser's output with the modulator.
26. The assembly of claim 1, wherein the photodetector includes an absorber.
5
27. The assembly of claim 26, wherein the photodetector includes a semiconductor optical amplifier.
28. The assembly of claim 26, wherein the photodetector includes at least one tunable filter.
10
29. The assembly of claim 26, wherein the photodetector includes a first and a second tunable filter.
10
30. The assembly of claim 29, wherein at least one of the first and second tunable filters is a distributed Bragg reflector.
15
31. The assembly of claim 29, wherein each of the first and second tunable filters is a distributed Bragg reflector.
15
32. The assembly of claim 29, wherein at least one of the first and second tunable filters is a sample-grating distributed Bragg reflector.
15
33. The assembly of claim 26, wherein the photodetector includes at least one electrical insulation area positioned adjacent to the absorber.
20
34. The assembly of claim 26, wherein the photodetector includes a pre-amplifier and a first electrical insulation area positioned between the pre-amplifier and the absorber.
20
35. The assembly of claim 26, wherein the photodetector includes a pre-amplifier and a first tunable filter positioned between the pre-amplifier and the absorber.
25
36. The assembly of claim 44, wherein the photodetector includes a second tunable filter.
25
37. The assembly of claim 36, wherein the first and second tunable filters define a resonant cavity.
30
38. A wavelength converter assembly, comprising:
a first semiconductor layer in an epitaxial structure;
a second semiconductor layer formed in the epitaxial structure, the first and second semiconductor layers having different dopings;
30

- a first waveguide layer formed between the first and second semiconductor layers, the first waveguide layer including a first reflector and a second reflector;
- an optically active gain medium disposed between the first and second reflectors, the first and second reflectors defining a resonant cavity;
- 5 a photodetector formed on the first semiconductor layer including an optically active absorber region, the photodetector generating a first electrical signal in response to an optical input.
39. The assembly of claim 38, further comprising:
- 10 a conditioning circuit coupled to the laser and the photodetector, the conditioning circuit receiving the first electrical signal and providing a second electrical signal to the laser to modulate its optical output.
40. The assembly of claim 39, wherein the conditioning circuit provides bias voltages to the photodetector and laser.
- 15 41. The assembly of claim 39, wherein the conditioning circuit contains nonlinear circuit elements to limit a magnitude of the second electrical signal wherein a maxima of signal pulses are reshaped.
42. The assembly of claim 3, wherein the conditioning circuit contains nonlinear circuit elements to supply a minimum level to the second electrical signal wherein a minima of signal pulses are reshaped.
- 20 43. The assembly of claim 38, wherein the laser includes a controllable phase shifting element.
44. The assembly of claim 38, wherein the gain medium includes multiple active regions.
- 25 45. The assembly of claim 44, wherein the multiple active regions are positioned along an optical axis defined by the first and second reflectors.
46. The assembly of claim 44, wherein the multiple active regions are positioned along an axis normal to an optical axis defined by the first and second reflectors.
- 30 47. The assembly of claim 38, wherein the first and second reflectors are tunable.
48. The assembly of claim 38, wherein at least one of the first and second reflectors is a distributed reflector.

49. The assembly of claim 38, wherein at least one of the first and second reflectors is a sample -grating distributed Bragg reflector.

50. The assembly of claim 38, wherein a maximum reflectivity of at least one of the first and second reflectors is tunable.

51. The assembly of claim 38, wherein a maximum reflectivity of each of the first and second reflectors is tunable.

52. The assembly of claim 51, wherein the maximum reflectivity of each of the first and second reflectors is tunable relative to each other.

53. The assembly of claim 38, wherein the laser includes a controllable amplifier positioned outside of the resonant cavity

54. The assembly of claim 38, wherein the laser includes a controllable modulator positioned outside of the resonant cavity.

55. The assembly of claim 38, wherein the laser includes a modulator and at least one amplifier positioned outside of the resonant cavity.

56. The assembly of claim 54, wherein the modulator is coupled to the photodetector.

57. The assembly of claim 38, wherein the photodetector includes an absorber.

58. The assembly of claim 57, wherein the photodetector includes a semiconductor optical amplifier.

59. The assembly of claim 57, wherein the photodetector includes at least one tunable filter.

60. The assembly of claim 57, wherein the photodetector includes a first and a second tunable filter.

61. The assembly of claim 60, wherein at least one of the first and second tunable filters is a distributed Bragg reflector.

62. The assembly of claim 60, wherein each of the first and second tunable filters is a distributed Bragg reflector.

63. The assembly of claim 60, wherein at least one of the first and second tunable filters is a sample-grating distributed Bragg reflector.

64. The assembly of claim 57, wherein the photodetector includes at least one electrical insulation area positioned adjacent to the absorber.

65. The assembly of claim 57, wherein the photodetector includes a pre-amplifier and a first electrical insulation area positioned between the pre-amplifier and the absorber.

5 66. The assembly of claim 57, wherein the photodetector includes a pre-amplifier and a first tunable filter positioned between the pre-amplifier and the absorber.

67. The assembly of claim 35, wherein the photodetector includes a second tunable filter.

10 68. A method of converting an optical wavelength, comprising:
providing a wavelength converter assembly with a photodetector and a laser with a common epitaxial structure with areas of differing bandgap, the laser including a laser resonator;

absorbing an optical input having a first wavelength at the wavelength converter assembly;

15 generating a first electrical signal from the photodetector in response to the optical input;

conditioning the first electrical signal and produce a conditioned first electrical signal;

20 generating a second electrical signal from the conditioned first electrical signal;

generating a laser output from a gain medium of the laser at a second wavelength in response to the second electrical signal.

69. The method of claim 68, wherein the wavelength converter assembly includes a current conditioning circuit coupled to the photodetector and the laser.

25 70. The method of claim 69, wherein the current conditioning circuit conditions the first electrical signal and produces the conditioned first electrical signal.

71. The method of claim 70, wherein the current conditioning circuit provides bias voltages to the photodetector and laser.

30 72. The method of claim 70, wherein the conditioning circuit contains nonlinear circuit elements to limit a magnitude of the second electrical signal wherein a maxima of signal pulses are reshaped.

73. The method of claim 70, wherein the conditioning circuit contains nonlinear circuit elements to supply a minimum level to the second electrical signal wherein a minima of signal pulses are reshaped.

74. The method of claim 73, wherein the substrate is semi-insulating
5 InP.

75. The method of claim 68, wherein conditioning the first electrical signal includes modifying the first electrical signal's bias and threshold.

76. The method of claim 68, wherein the optical input is absorbed at the photodetector and a gain from the gain medium occur at the common
10 epitaxial structure.

77. The method of claim 68, wherein the optical input is absorbed at the photodetector and a gain from the gain medium occur at a common level of the common epitaxial structure.

78. The method of claim 68, further comprising:
15 controlling a phase of the laser output.

79. The method of claim 68, wherein the laser has a first reflector and a second reflector that define the laser resonator, wherein at least one of the first and second reflectors is frequency selective and tunable..

80. The method of claim 79, further comprising:
20 tuning a maximum reflectivity of the first reflector relative to a maximum reflectivity of the second reflector to select the second wavelength.

81. The method of claim 68, further comprising:
modulating the laser output.

82. The method of claim 68, wherein the second electrical signal
25 modulates the laser's output.

83. The method of claim 86, wherein the laser output is modulated outside the laser resonator at the common epitaxial structure.

84. The method of claim 68, further comprising:
selecting a range of wavelengths for detection at the photodetector .

85. The method of claim 68, further comprising:
30 amplifying the optical input prior to absorption by the wavelength converter assembly.

86. A method of converting an optical wavelength, comprising:

providing a wavelength converter assembly having an epitaxial structure with areas of differing bandgap that includes a waveguide layer positioned between first and second semiconductor layers of the epitaxial structure, an optically active gain medium positioned between first and second reflectors that define a resonant cavity, and a photodetector;

5 detecting an optical input at the photodetector; and

 generating a laser output from the wavelength converter assembly in response to the optical input.

87. The method of claim 86, wherein the optical input has a first wavelength.

88. The method of claim 87, further comprising:
generating a first electrical signal from the photodetector in response to
the optical input.

15 89. The method of claim 88, further comprising:
conditioning the first electrical signal and produce a conditioned first
electrical signal.

90. The method of claim 89, further comprising:
generating a second electrical signal from the conditioned first electrical
signal.

20 91. The method of claim 90, further comprising:
providing bias voltages to the photodetector and laser

92. The method of claim 90, further comprising:
limiting a magnitude of the second electrical signal; and
reshaping a maxima of signal pulses.

25 93. The method of claim 70, further comprising:
 supplying a minimum level to the second electrical signal; and
 reshaping a minima of signal pulses.

94. The method of claim 90, further comprising:
generating the laser output from a gain medium of the laser at a second
wavelength in response to the second electrical signal.

95. The method of claim 89, wherein the wavelength converter assembly includes a current conditioning circuit coupled to the photodetector and the laser.

96. The method of claim 95, wherein the current conditioning circuit conditions the first electrical signal and produces the conditioned first electrical signal.

5 97. The method of claim 86, further comprising:
controlling a phase of the laser output.

98. The method of claim 86, further comprising:
tuning a maximum reflectivity of the first reflector relative to a
maximum reflectivity of the second reflector to select the laser output.

10 99. The method of claim 86, further comprising:
modulating the laser output.

100. The method of claim 68, wherein the second electrical signal
modulates the laser's output.

101. The method of claim 99, wherein the laser output is modulated
outside the resonant cavity at the common epitaxial structure.

15 102. The method of claim 86, further comprising:
selecting a range of wavelengths for detection at the photodetector .

103. The method of claim 86, further comprising:
amplifying the optical input prior to prior to detecting the optical input.

104. A method of making a wavelength converter assembly,
20 comprising:

providing a substrate;

forming an epitaxial structure on the substrate, wherein different areas of
the epitaxial structure have different optical properties;

forming a laser in the epitaxial structure;

25 forming a photodetector in the epitaxial structure.

105. The method of claim 104, further comprising:
forming a conditioning circuit coupled to the laser and the photodetector
on the substrate, the conditioning circuit receiving a first electrical signal from
the photodetector and providing a second electrical signal to the laser to
modulate its optical output.

30 106. The method of claim 105, wherein the conditioning circuit
provides necessary bias voltages to the photodetector and laser.

107. The method of claim 106, wherein the conditioning circuit contains nonlinear circuit elements to limit a magnitude of the second electrical signal wherein a maxima of signal pulses are reshaped.

108. The method of claim 106, wherein the conditioning circuit
5 contains nonlinear circuit elements to supply a minimum level to the second electrical signal wherein a minima of signal pulses are reshaped.

109. The method of claim 104, wherein the substrate is semi-insulating InP.

110. The method of claim 104, further comprising:
10 forming areas of different bandgaps in the epitaxial structure.

111. The method of claim 104 further comprising:
bombarding at least a portion of the epitaxial structure with ions; and annealing the epitaxial structure to diffuse impurities and vacancies in a selected region of the epitaxial structure to determine the region's optical properties.

112. The method of claim 104, wherein at least a portion of the surface of the epitaxial structure is bombarded with the ions.

113. The method of claim 111, wherein the ions have an energy no greater than about 200 eV.

114. The method of claim 104, wherein the photodetector has at least
20 one bandgap that is different from at least one bandgap of the laser.

115. The method of claim 104, wherein the laser includes a mode tuning element.

116. The method of claim 115, wherein the mode tuning element is a controllable phase shifting element.

25 117. The method of claim 104, wherein the laser includes a first reflector and a second reflector that define a resonant cavity, wherein at least one of the first and second reflectors is frequency selective and tunable.

118. The method of claim 117, wherein at least one of the first and second reflectors is a distributed reflector.

30 119. The method of claim 117, wherein both of the first and second reflectors is a distributed reflector.

120. The method of claim 117, wherein at least one of the first and second reflectors is a distributed Bragg reflector.

121. The method of claim 117, wherein at least one of the first and second reflectors is a sampled-grating distributed Bragg reflector.

122. The method of claim 117, wherein each of the first and second reflectors is a distributed Bragg reflector.

5 123. The method of claim 117, wherein each of the first and second reflectors is a sampled-grating distributed Bragg reflector.

124. The method of claim 117, wherein a maximum reflectivity of at least one of the first and second reflectors is tunable.

10 125. The method of claim 117, wherein a maximum reflectivity of each of the first and second reflectors is tunable.

126. The method of claim 117, wherein the maximum reflectivities of each of the first and second reflectors are tunable relative to each other.

127. The method of claim 1, wherein the laser has a gain medium that is coupled to the photodetector.

15 128. The method of claim 104, wherein the laser has a multi-active region gain medium.

129. The method of claim 117, wherein the laser includes a controllable amplifier positioned outside of the resonant cavity

20 130. The method of claim 117, wherein the laser includes a controllable modulator positioned outside of the resonant cavity.

131. The method of claim 117, wherein the laser includes a modulator and at least one amplifier positioned outside of the resonant cavity.

25 132. The method of claim 130, wherein the modulator is coupled to the photodetector wherein the second electrical signal modulates the laser's output with the modulator.

133. The method of claim 131, wherein the modulator is coupled to the photodetector wherein the second electrical signal modulates the laser's output with the modulator.

30 134. The method of claim 104, wherein the photodetector includes an absorber.

135. The method of claim 134, wherein the photodetector includes a semiconductor optical amplifier.

136. The method of claim 134, wherein the photodetector includes at least one tunable filter.

137. The method of claim 134, wherein the photodetector includes a first and a second tunable filter.

5 138. The method of claim 146, wherein at least one of the first and second tunable filters is a distributed Bragg reflector.

139. The method of claim 146, wherein each of the first and second tunable filters is a distributed Bragg reflector.

10 140. The method of claim 146, wherein at least one of the first and second tunable filters is a sampled-grating distributed Bragg reflector.

141. The method of claim 134, wherein the photodetector includes at least one electrical insulation area positioned adjacent to the absorber.

15 142. The method of claim 134, wherein the photodetector includes a pre-amplifier and a first electrical insulation area positioned between the pre-amplifier and the absorber.

143. The method of claim 134, wherein the photodetector includes a pre-amplifier and a first tunable filter positioned between the pre-amplifier and the absorber.

20 144. The method of claim 143, wherein the photodetector includes a second tunable filter.

145. The method of claim 144, wherein the first and second tunable filters define a resonant cavity.

25 146. A method of making a wavelength converter assembly, comprising:
providing a substrate;
forming an epitaxial structure on the substrate;
bombarding at least a portion of the epitaxial structure with ions;
annealing the epitaxial structure to diffuse impurities and vacancies in a selected region of the epitaxial structure to determine the region's optical properties; and
30 creating a laser and a photodetector in the epitaxial structure.

147. The method of claim 146, further comprising:

forming a conditioning circuit coupled to the laser and the photodetector on the substrate, the conditioning circuit receiving a first electrical signal from

the photodetector and providing a second electrical signal to the laser to modulate its optical output.

148. The method of claim 147, wherein the conditioning circuit provides necessary bias voltages to the photodetector and laser.

5 149. The method of claim 147, wherein the conditioning circuit contains nonlinear circuit elements to limit a magnitude of the second electrical signal wherein a maxima of signal pulses are reshaped.

10 150. The method of claim 147, wherein the conditioning circuit contains nonlinear circuit elements to supply a minimum level to the second electrical signal wherein a minima of signal pulses are reshaped.

151. The method of claim 146, wherein the substrate is semi-insulating InP.

152. The method of claim 146, further comprising:
forming areas of different bandgaps in the epitaxial structure.

153. The method of claim 146, wherein at least a portion of the surface of the epitaxial structure is bombarded with the ions.

154. The method of claim 147, wherein the ions have an energy no greater than about 200 eV.

155. The method of claim 146, wherein the photodetector has at least one bandgap that is different from at least one bandgap of the laser.

156. The method of claim 146, wherein the laser includes a mode tuning element.

157. The method of claim 156, wherein the mode tuning element is a controllable phase shifting element.

25 158. The method of claim 146, wherein the laser includes a first reflector and a second reflector that define a resonant cavity, wherein at least one of the first and second reflectors is tunable.

159. The method of claim 158, wherein at least one of the first and second reflectors is a distributed reflector.

30 160. The method of claim 158, wherein both of the first and second reflectors is a distributed reflector.

161. The method of claim 158, wherein at least one of the first and second reflectors is a distributed Bragg reflector.

162. The method of claim 161, wherein at least one of the first and second reflectors is a sampled-grating distributed Bragg reflector.

163. The method of claim 158, wherein each of the first and second reflectors is a distributed Bragg reflector.

5 164. The method of claim 158, wherein a maximum reflectivity of at least one of the first and second reflectors is tunable.

165. The method of claim 158, wherein a maximum reflectivity of each of the first and second reflectors is tunable.

10 166. The method of claim 158, wherein the maximum reflectivities of each of the first and second reflectors are tunable relative to each other.

167. The method of claim 146, wherein laser has a gain medium that is coupled to the photodetector.

168. The method of claim 146, wherein the laser has a multi-active region gain medium.

15 169. The method of claim 158, wherein the laser includes a controllable amplifier positioned outside of the resonant cavity

170. The method of claim 158, wherein the laser includes a controllable attenuator positioned outside of the resonant cavity.

171. The method of claim 158, wherein the laser includes an attenuator and at least one amplifier positioned outside of the resonant cavity.

172. The method of claim 146, wherein the photodetector includes an absorber.

173. The method of claim 146, wherein the photodetector includes a semiconductor optical amplifier.

25 174. The method of claim 146, wherein the photodetector includes at least one tunable filter.

175. The method of claim 146, wherein the photodetector includes a first and a second tunable filter.

176. The method of claim 175, wherein at least one of the first and second tunable filters is a distributed Bragg reflector.

30 177. The method of claim 175, wherein each of the first and second tunable filters is a distributed Bragg reflector.

178. The method of claim 146, wherein the photodetector includes at least one electrical insulation area positioned adjacent to the absorber.

179. The method of claim 146, wherein the photodetector includes a pre-amplifier and a first electrical insulation area positioned between the pre-amplifier and the absorber.

5 180. The method of claim 146, wherein the photodetector includes a pre-amplifier and a first tunable filter positioned between the pre-amplifier and the absorber.

10 181. The method of claim 146, wherein the photodetector includes a second tunable filter.

182. The method of claim 161, wherein the first and second tunable filters define a resonant cavity.

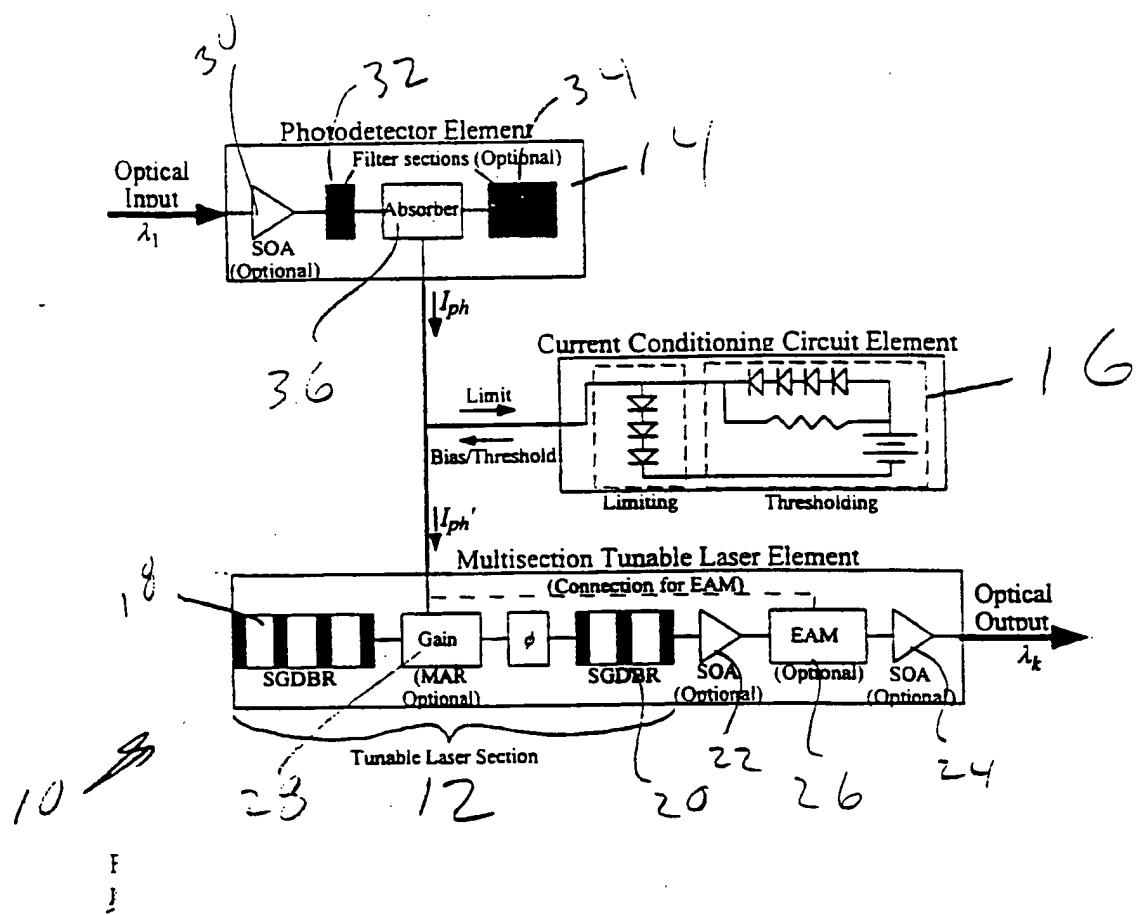


Fig. 1

Fig 2(a)

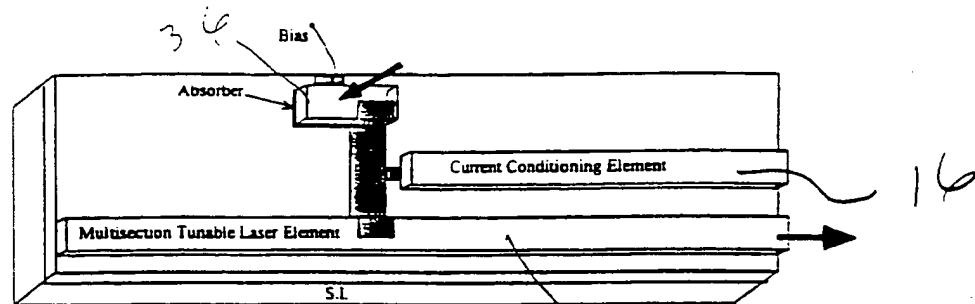


Fig 2(b)

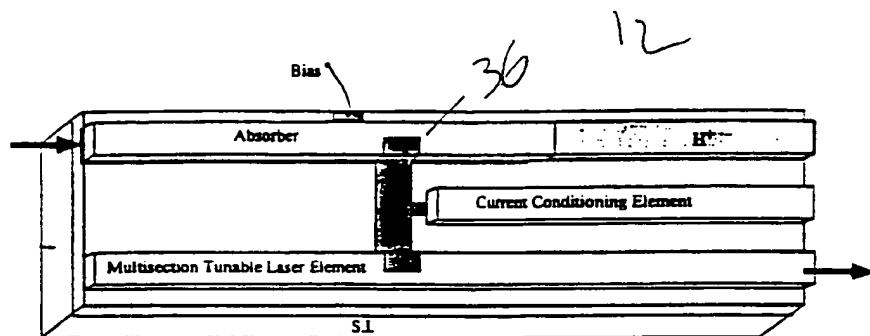


Fig 2(c)

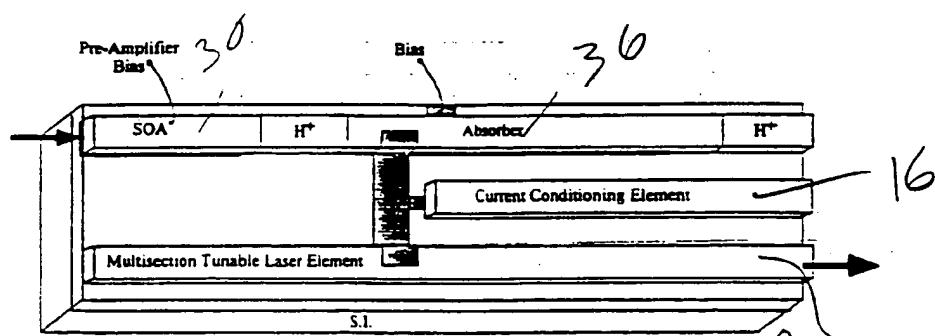
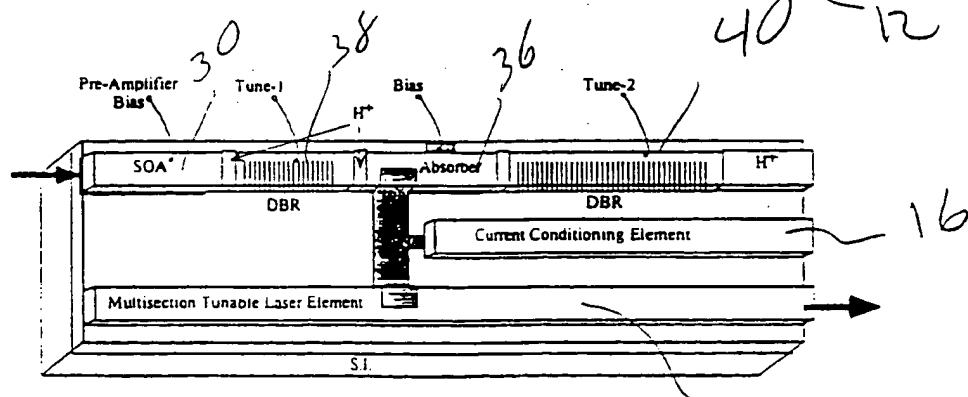


Fig 2(d)



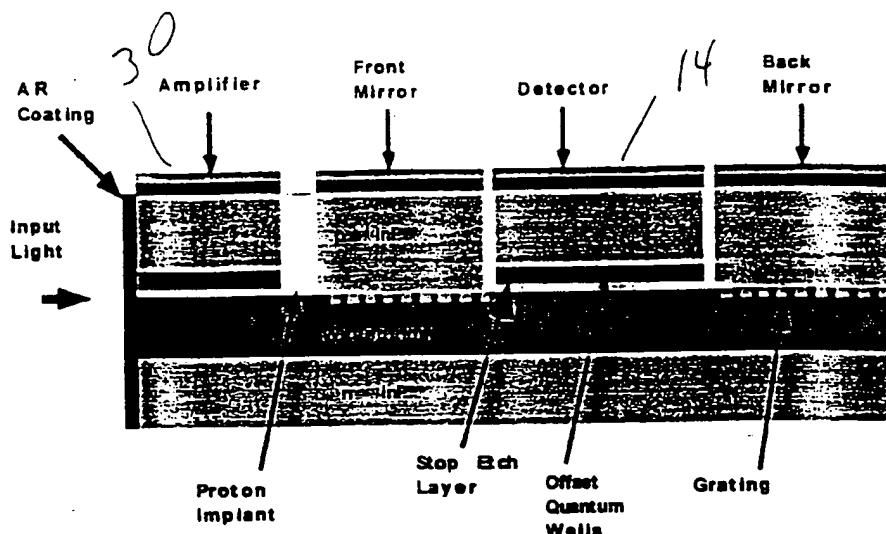


Figure 3a.

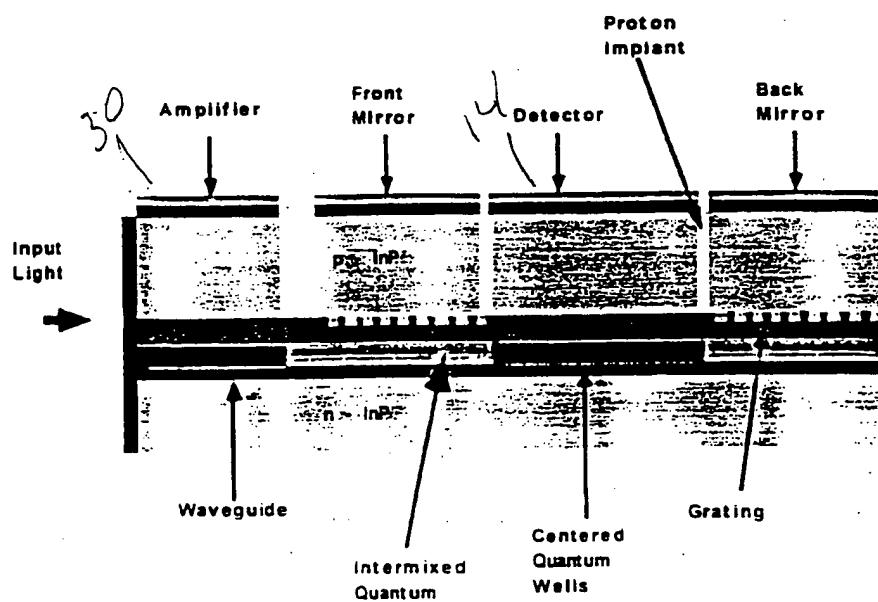
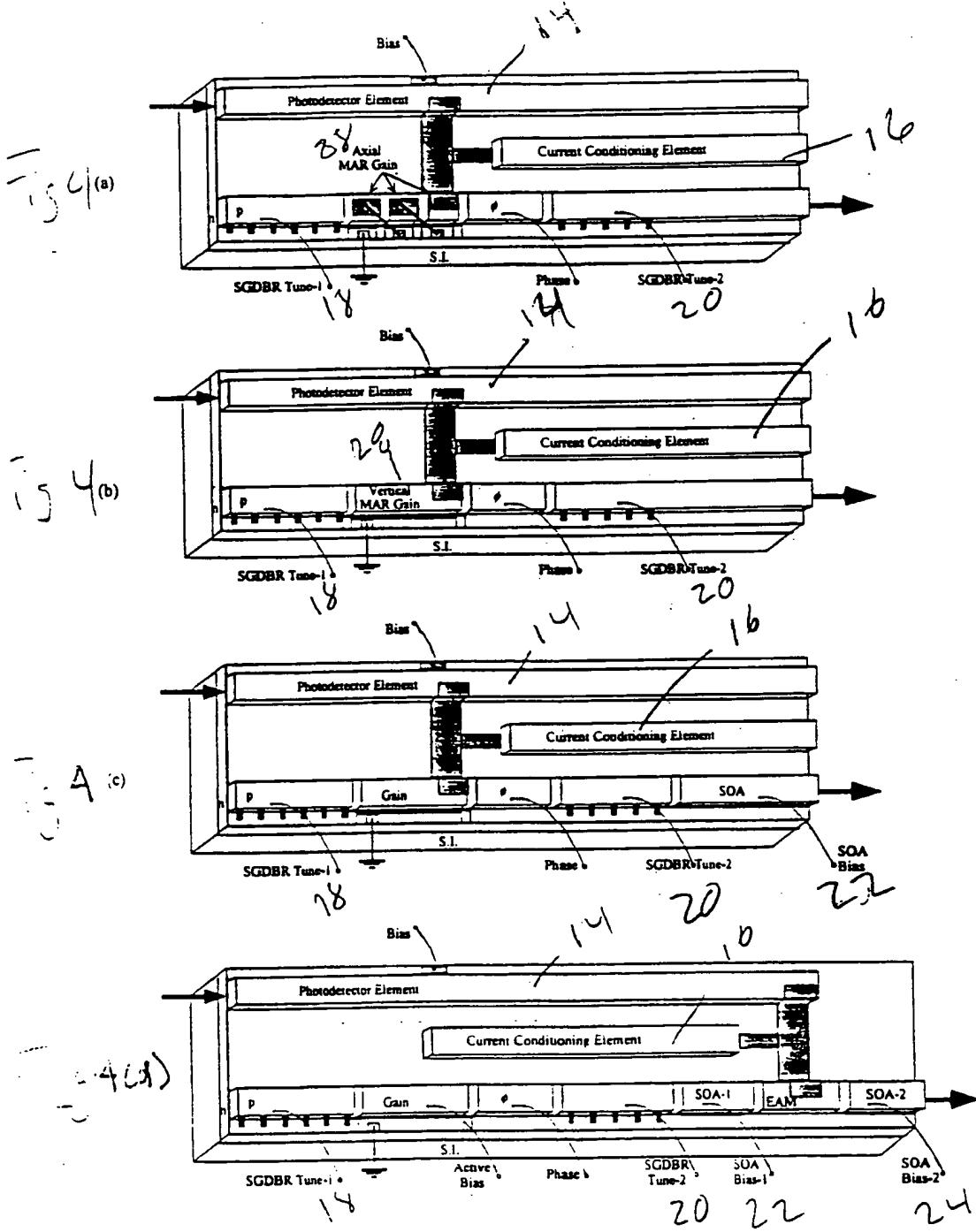


Figure 3b.



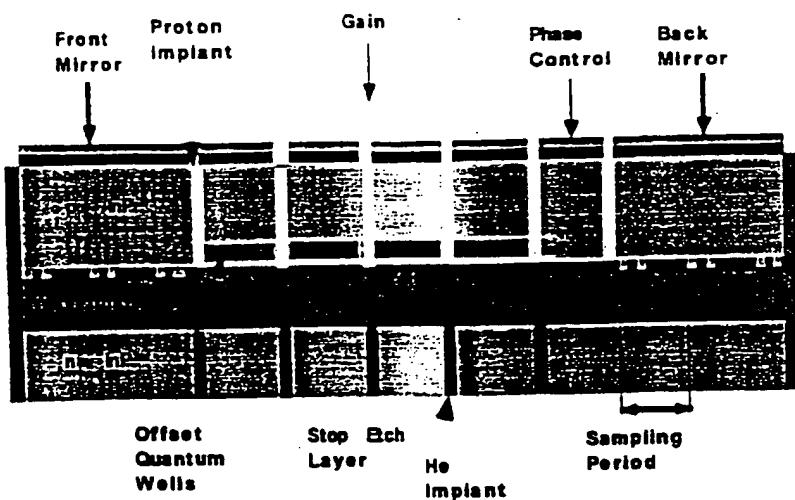


Figure 5a.

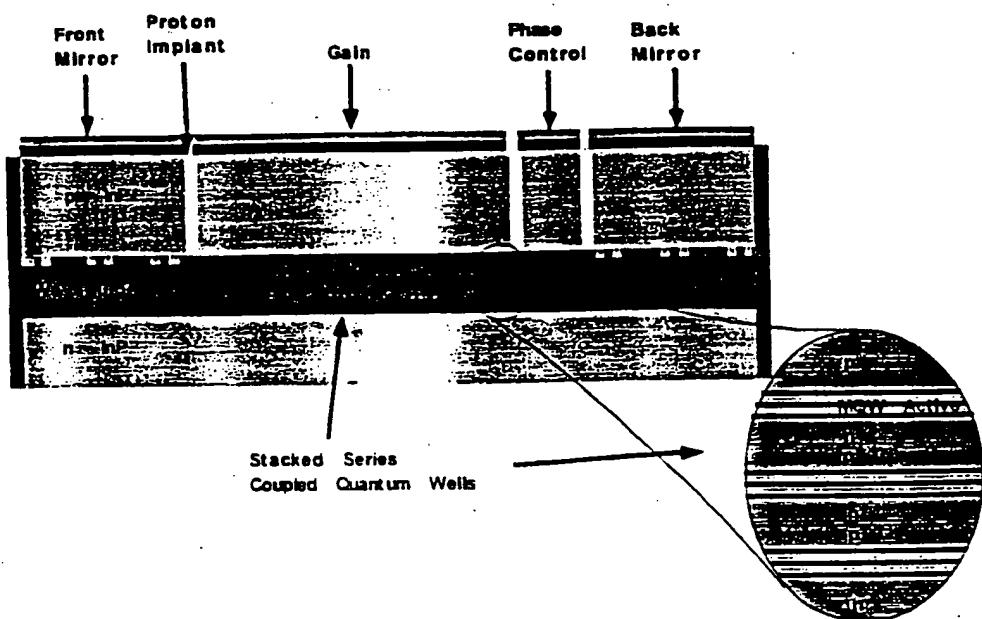


Figure 5b..

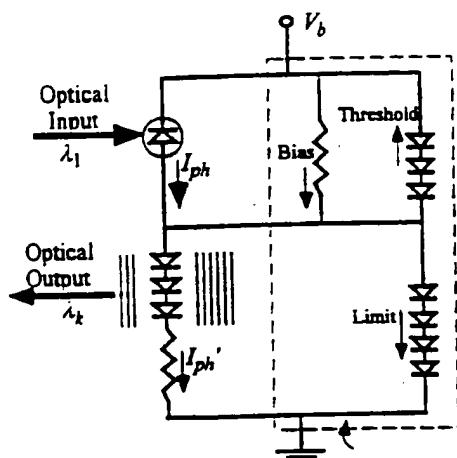


Figure 6

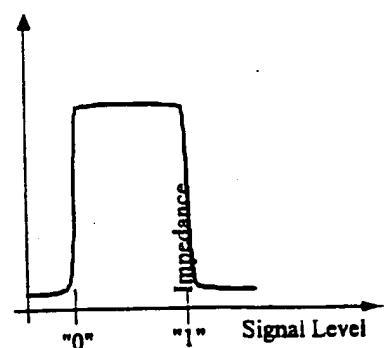


Figure 7

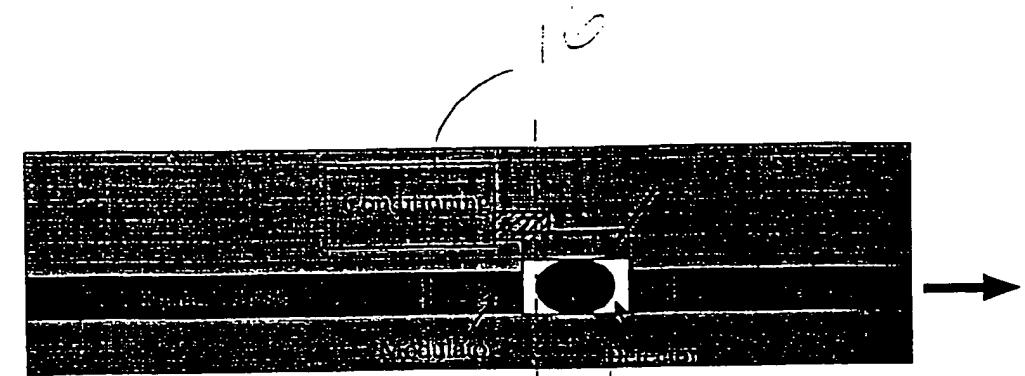


Fig 8(a)

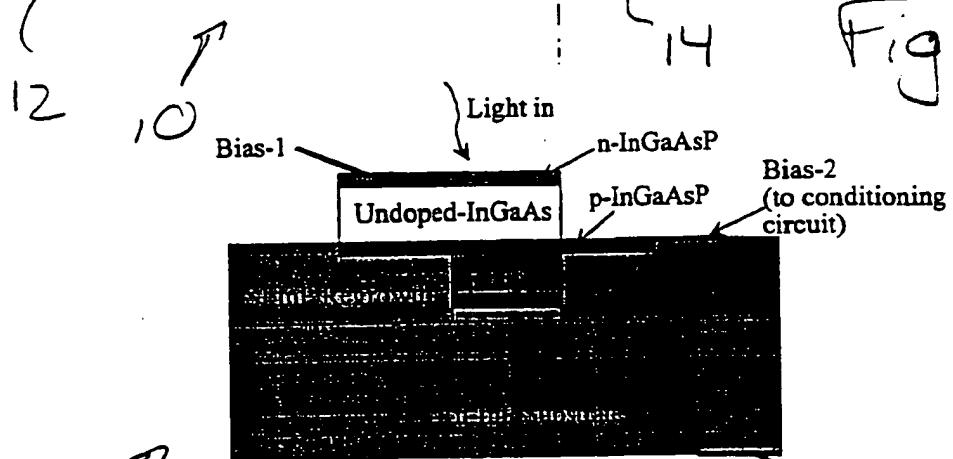


Fig 8(b)